

Low Profile Tunable Dipole Antennas Using BST Varactors for Biomedical Applications

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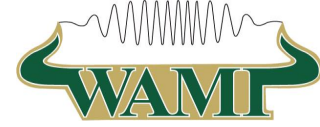
Outline

- Motivation
- Background
- Previous Related Work
- 1-D Varactor based Tunable Antenna
- Summary
- Acknowledgement
- References

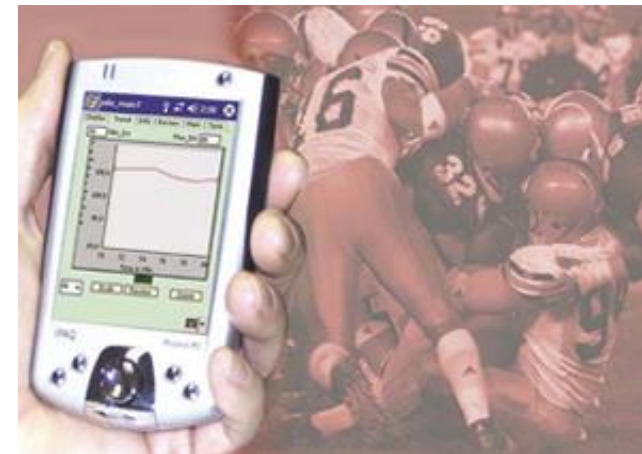
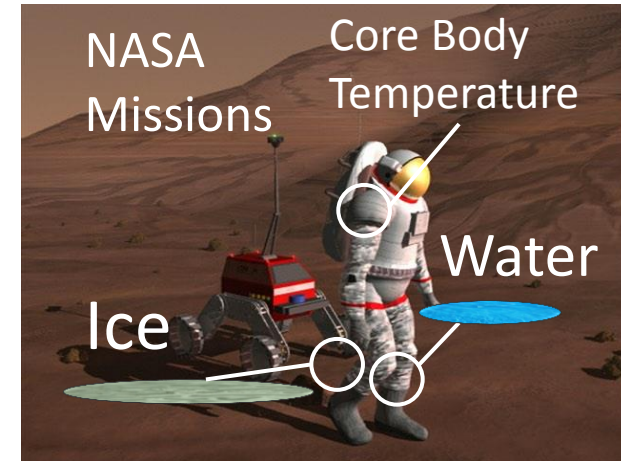
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MOTIVATION

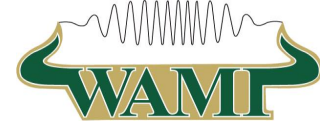
Motivation



- Design a low profile, conformal, tunable antenna for biomedical applications
- Portable radiometer applications:
 - Health monitoring sensor – astronauts, sports medicine, etc.
 - Remote Underground Thermal Detection

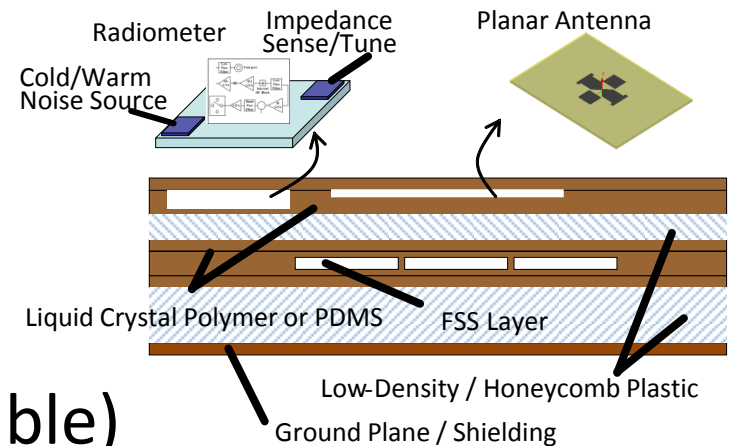
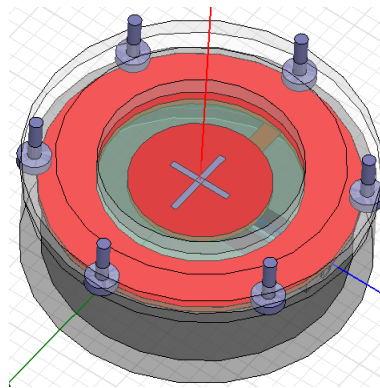


Motivation(Cont.)



- Antenna Requirements for wearable radiometer:
 - Minimize back-side radiation
 - Large bandwidth (~ 100 MHz)
 - Low profile and conformal (flexible)
 - Low weight, low cost & low complexity

27 mm height
 $\sim \lambda/8$ at 1.4 GHz



Cavity-Backed Slot
Antenna (CBSA)*
Cons: Bulky, heavy.

[*] Q. Bonds, T. Weller, B. Roeder and P. Herzig, "A tunable Cavity Backed Slot Antenna (CBSA) for close proximity biomedical sensing applications," in IEEE Microwaves, Communications, Antennas and Electronics Systems, 2009

Low Profile Tunable Dipole Antennas
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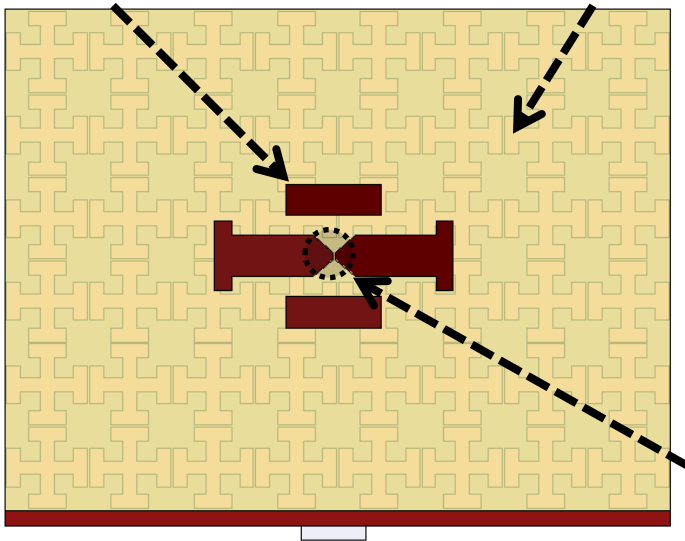
PREVIOUS WORKS

Antenna Structure

Top View

Dipole

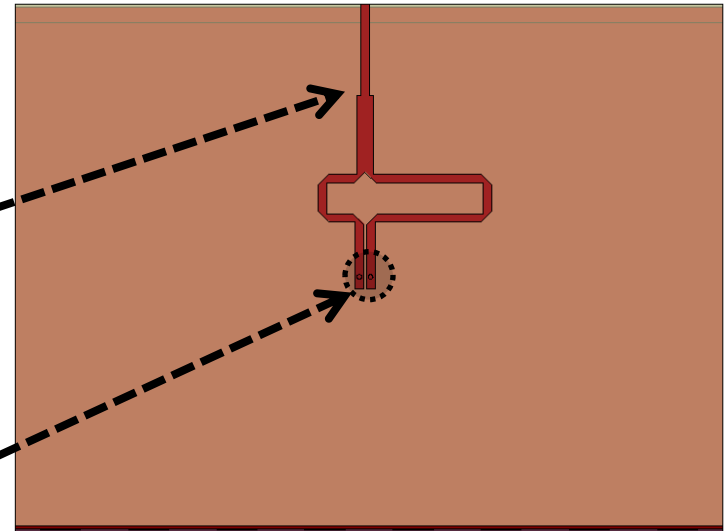
High Impedance Surface



Bottom View

Balun

Live vias

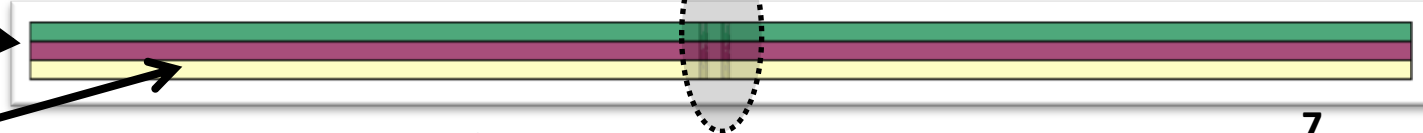


Side View

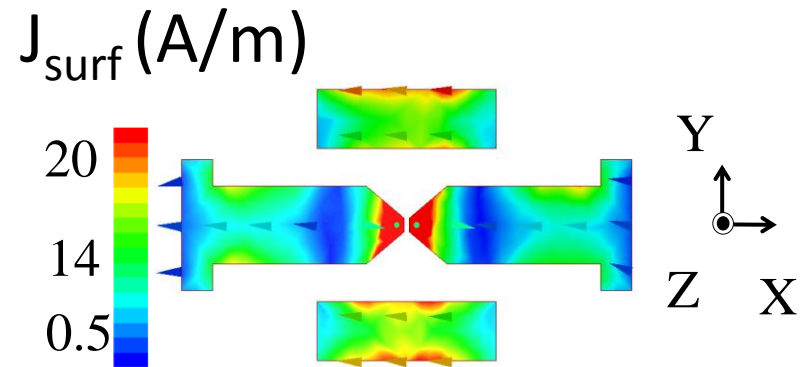
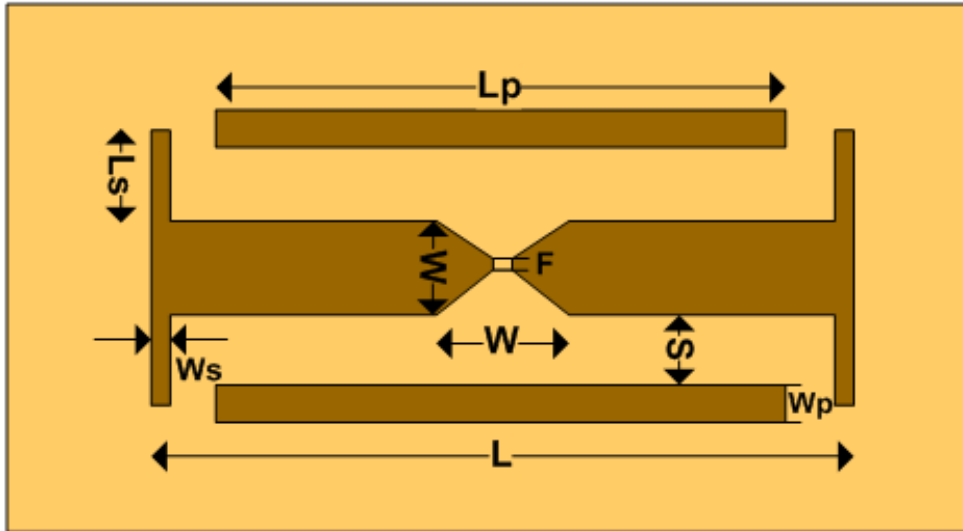
Dipole-Layer 1

HIS -layer 2

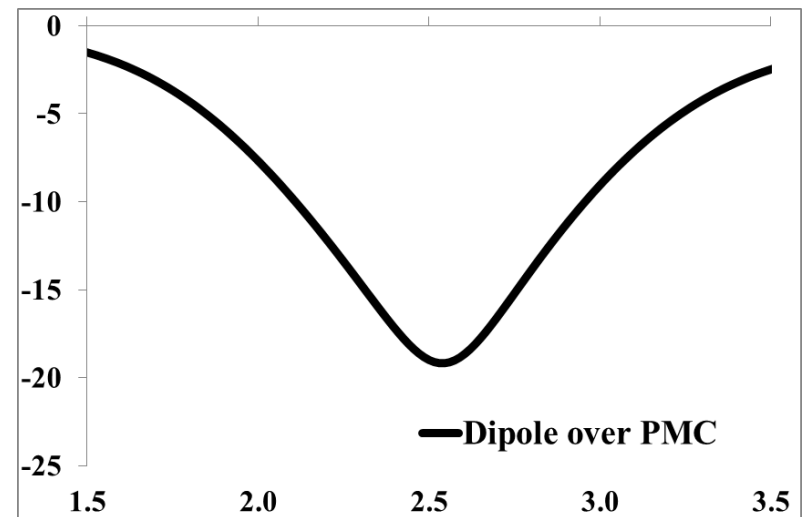
Balun – Layer 3



Dipole

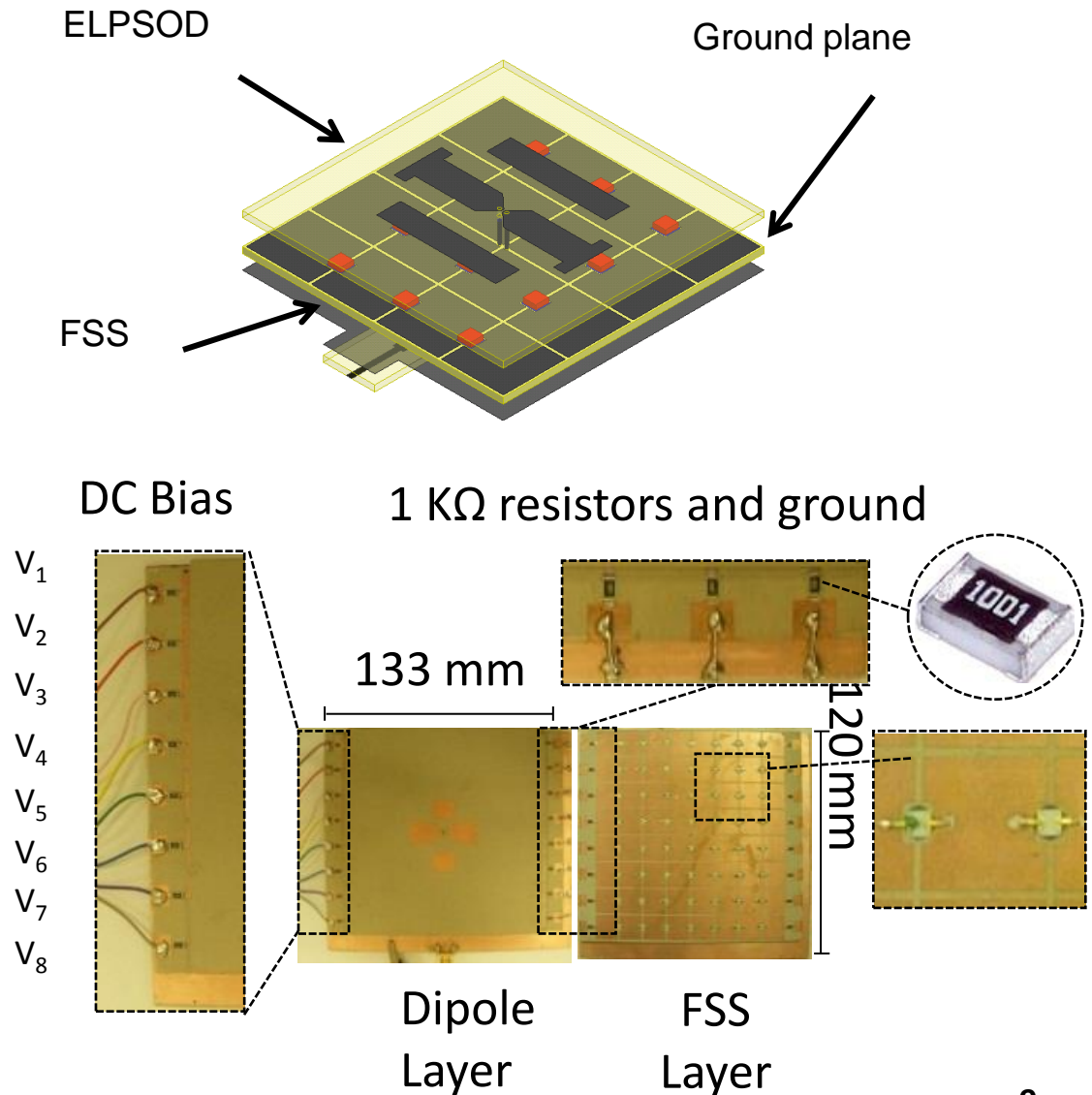


- End-Loaded Planar Open-Sleeve (ELPOSD)
- Broadband or dual response
- Tunable: Several parameters
- L_p affects the upper resonance frequency
- L affects the Lower resonance frequency

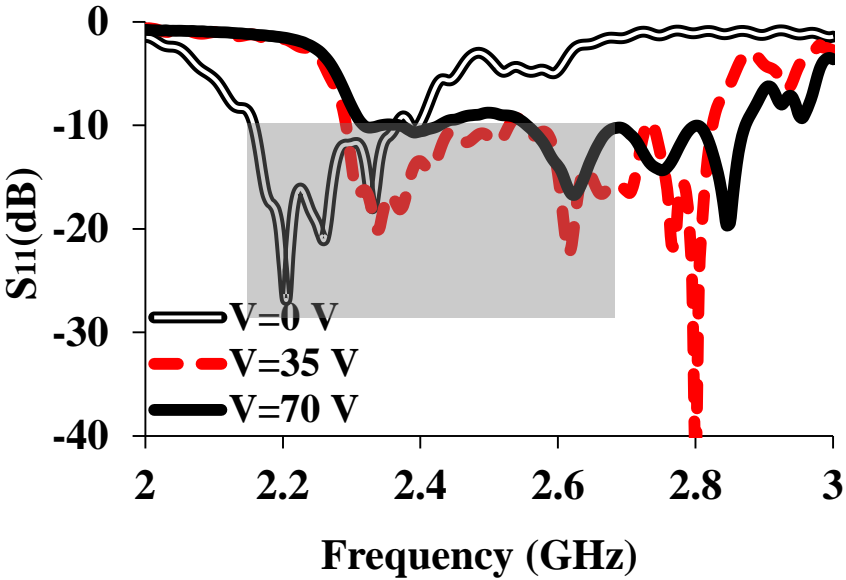


1-D Varactor based Tunable Antenna

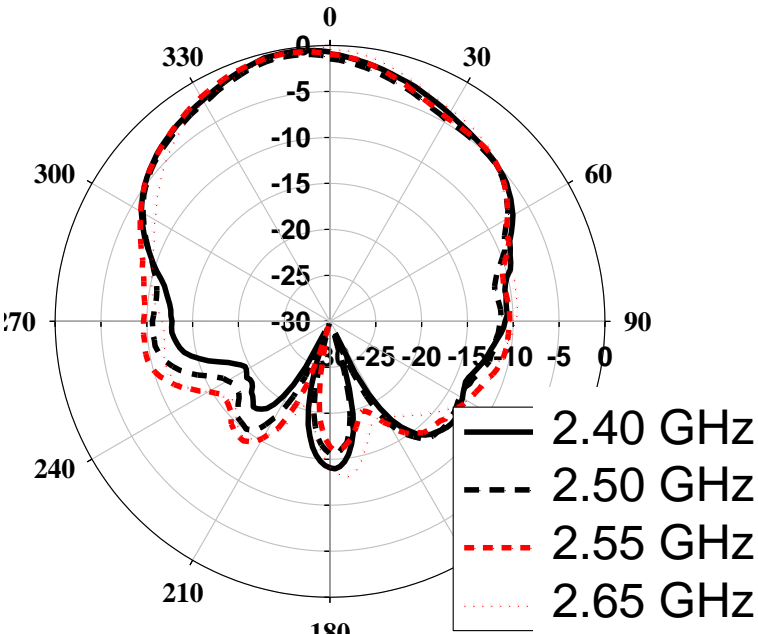
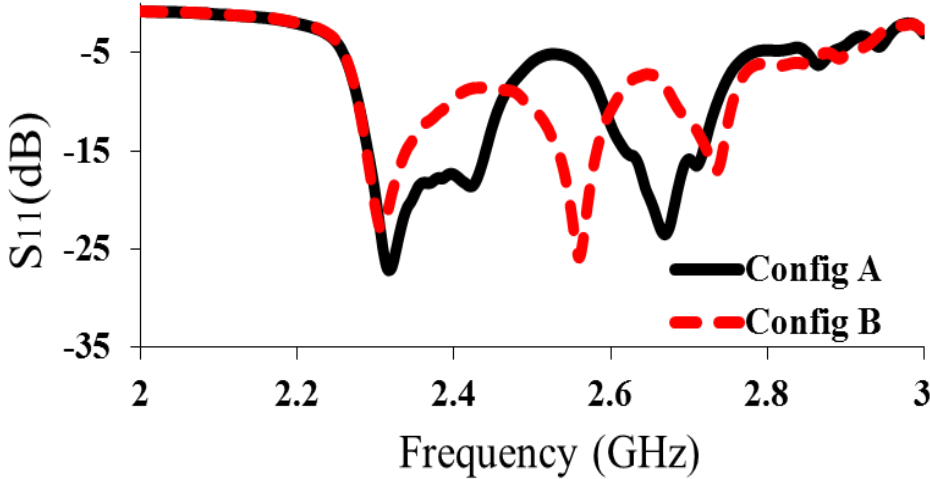
- Height $\sim \lambda/45$ at 2.4 GHz
- Bias and fabrication simplicity
- Minimize the use of vias (potentially conformal nature)
- High front-to-back radiation pattern ratio
- Ability to dynamically adjust the center frequency



Common bias applied



Non-uniform bias voltages

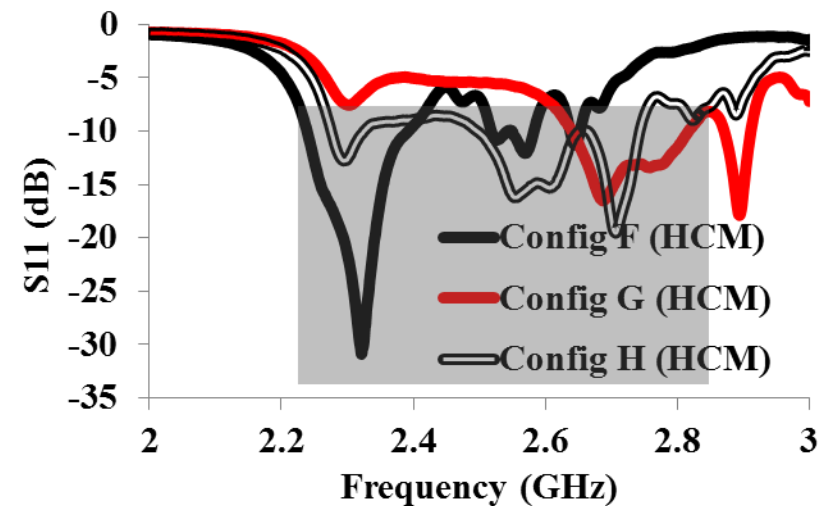
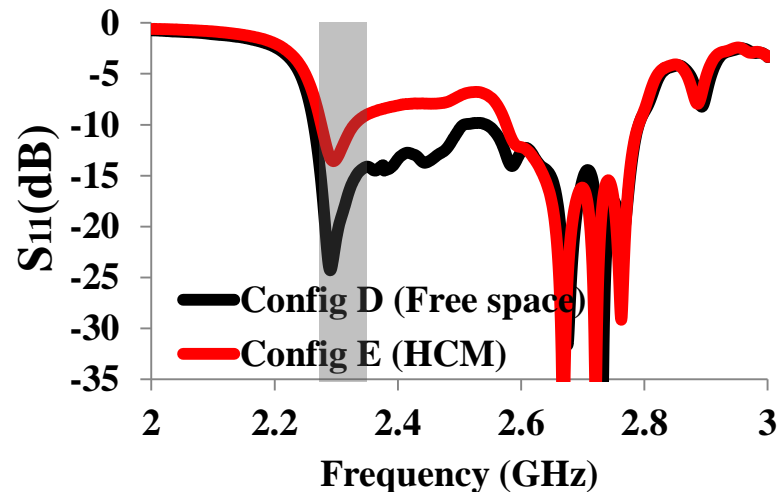


Config	V_1, V_2	V_3	V_4, V_5	V_6	V_7, V_8
A	30 V	30 V	30 V	30 V	30 V
B	70 V	70 V	30 V	70 V	70 V

Operation using non-uniform bias voltages with Human Core Model (HCM)



Config.	V_1, V_2	V_3	V_4, V_5	V_6	V_7, V_8
D (No HCM)	30 V	30 V	30 V	30 V	30 V
E (w/ HCM)	30 V	30 V	30 V	30 V	30 V
F (w/ HCM)	10 V	30 V	30 V	30 V	20 V
G (w/ HCM)	50 V	30 V	30 V	30 V	50 V
H (w/ HCM)	100 V	100 V	100 V	100 V	100 V

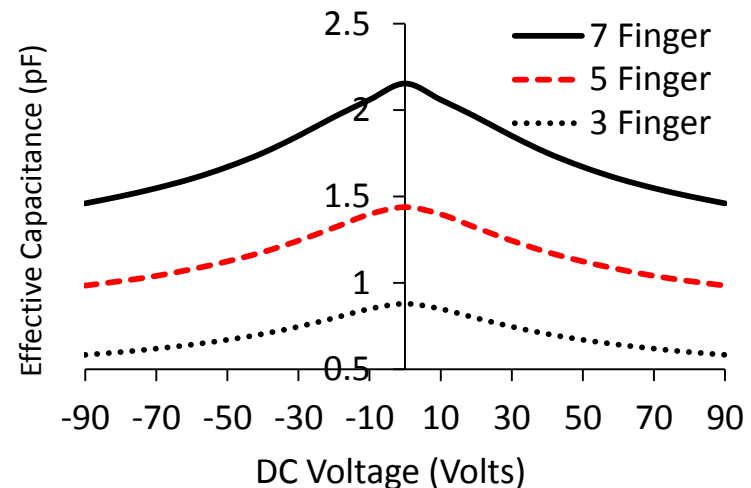
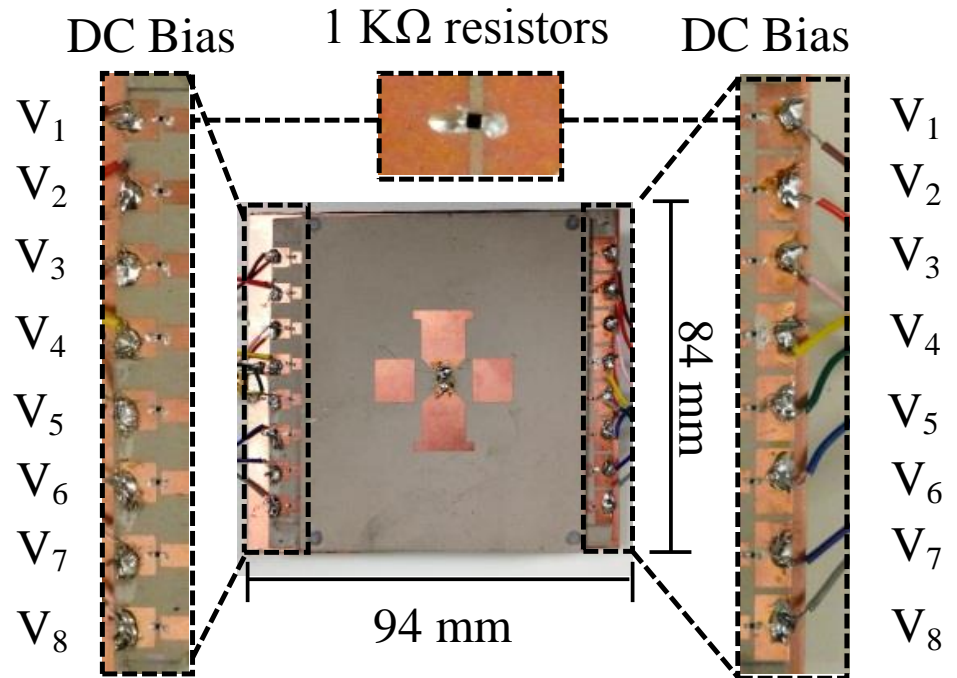


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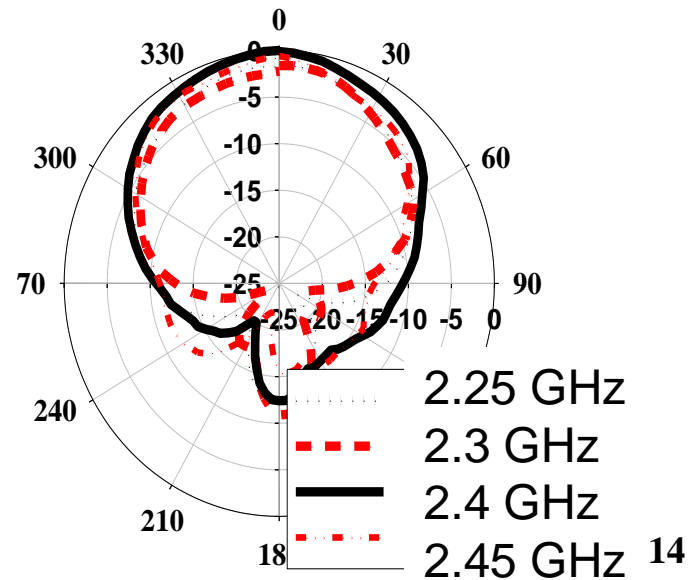
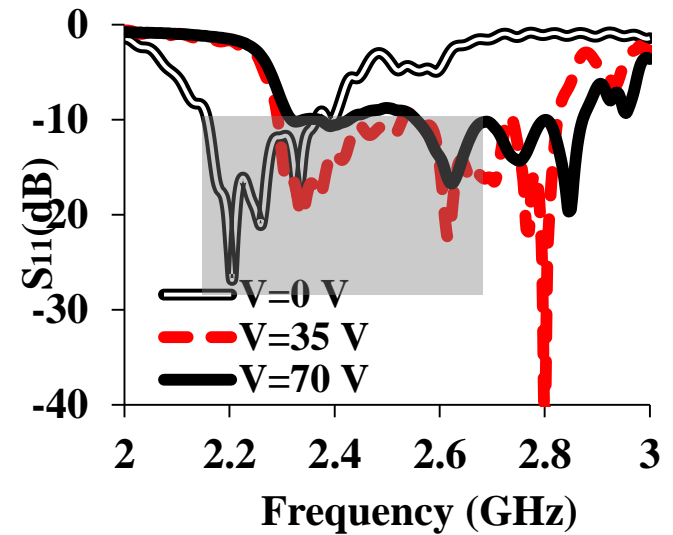
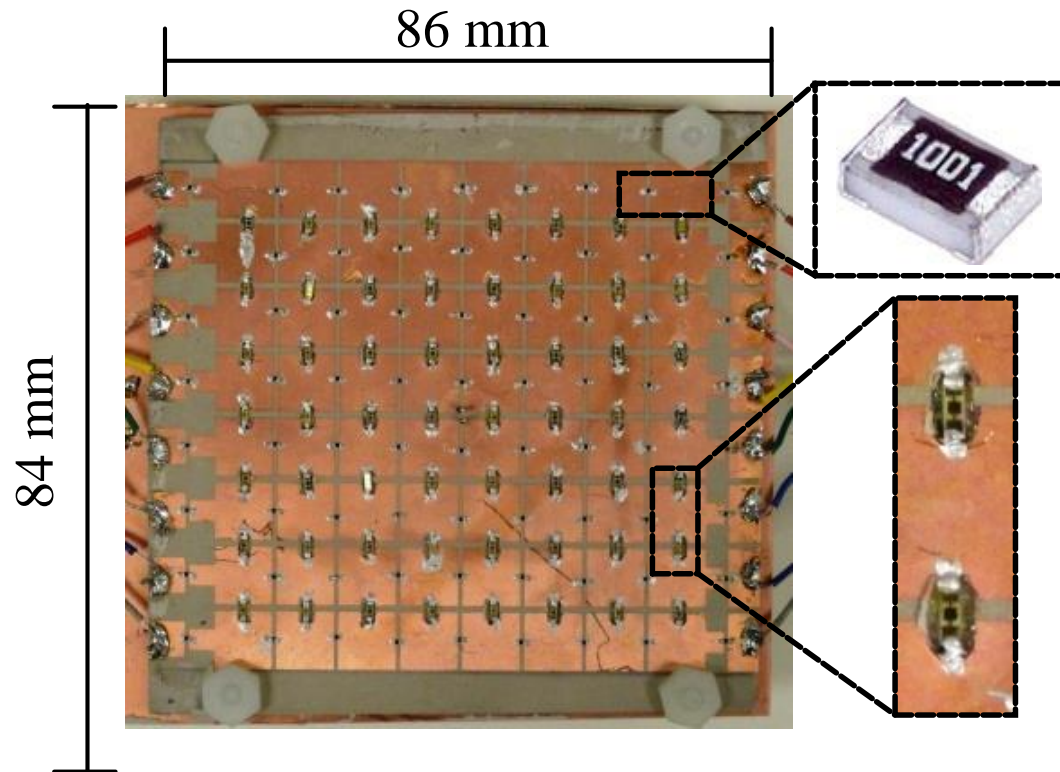
1-D BST VARACTOR BASED ANTENNA

BST Varactor Based antenna

- Height $\sim \lambda/45$ at 2.4 GHz
- Bias and fabrication simplicity
- Take advantage of the C-V symmetry curve
- Avoid the use of vias (potentially conformal nature)
- High front-to-back radiation pattern ratio
- Ability to dynamically adjust the center frequency



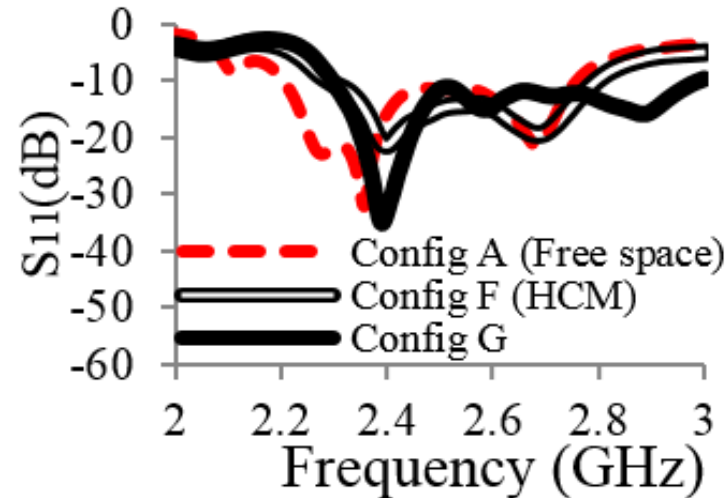
FSS Layer Using Barium Strontium Titanate (BST) Varactors



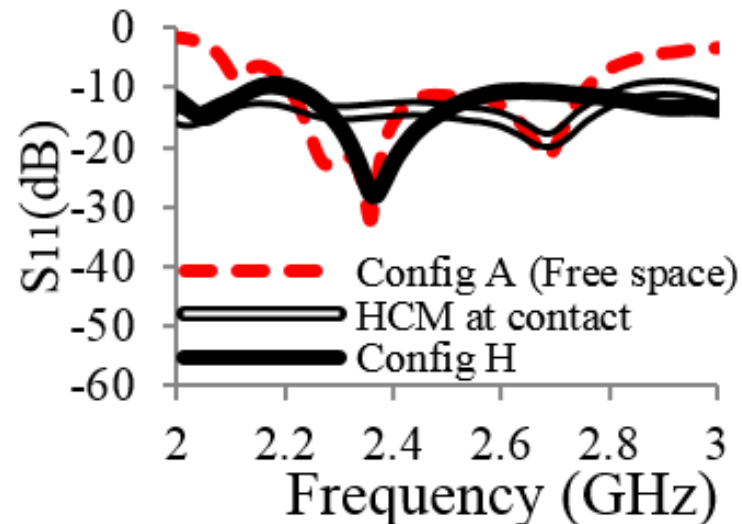
Operation using non-uniform bias voltages with Human Core Model (HCM)

Impedance match adjustment in:

- Close proximity to a HMC



- At contact with HMC



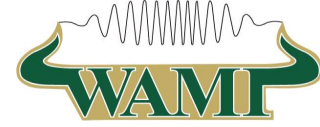
GaAs vs. BST antenna

Antenna	Mass (gms)	Total devices	Cost per device	Cost	Area (mm ²)	Eff. (%)	Tunable BW (MHz)
GaAs	188	56	50 US\$	High	15600	50-80	520
BST	87	56	0.1 US\$	Low	7900	30-60	425

■ GaAs vs BST varactor based antenna

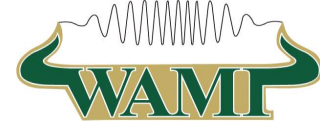
- Both - low profile
- Both - Easily tunable
- BST - Reduced planar size and mass compared to GaAs
- BST- Cost effective
- BST - Compact and robust

Summary



- A low profile, tunable dipole antenna using BST varactors has been demonstrated
- The total antenna thickness is $\sim \lambda/45$ when using 1-D varactor-loading
- A tunable frequency response from 2.2 to 2.55 GHz
- Cost effective, compact, robust, easily tunable and low profile antenna
- BST varactor antenna enables:
 - Small bias Network voltages
 - Potential use of flexible substrates

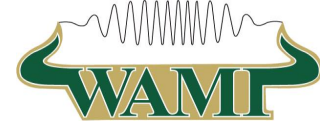
Acknowledgment



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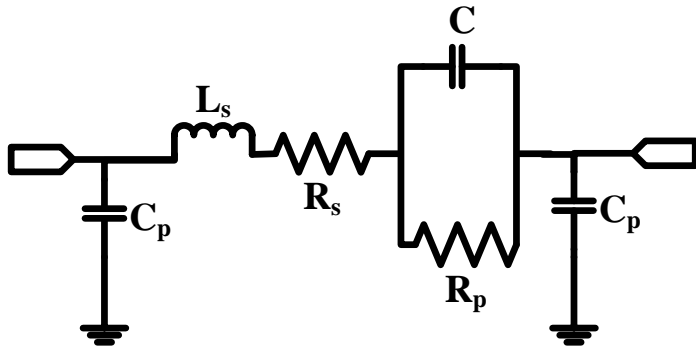


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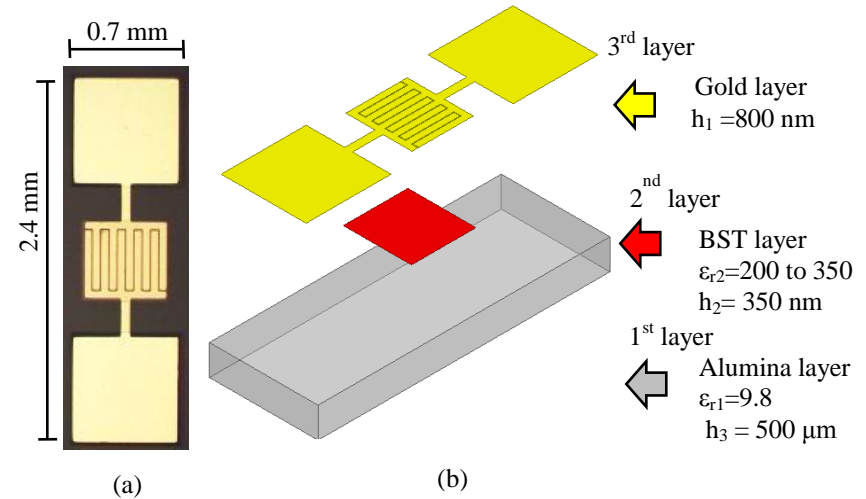
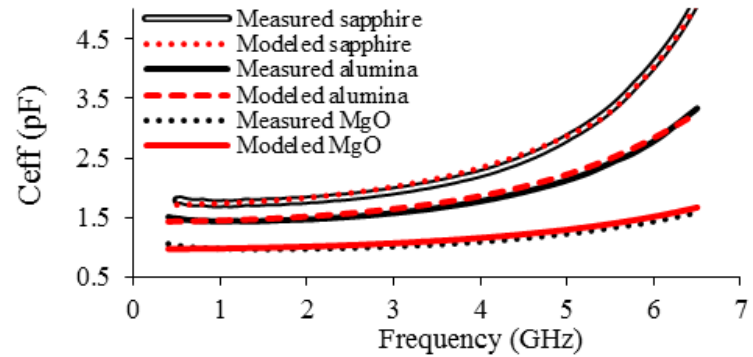
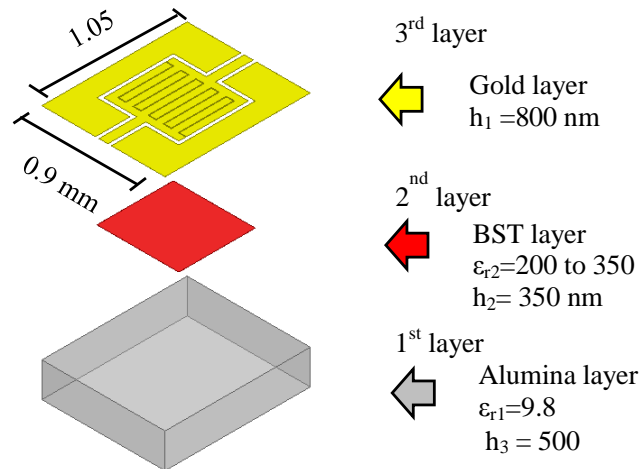
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Add. 1 BST Varactor Characterization



Schematic for diode simulation.



Add. 2

$$C_{end} = 4ns(2 + \pi)\epsilon_{end}\epsilon_0 \frac{K(\kappa_{0end})}{K(\kappa'_{0end})} \quad \begin{matrix} 54\% \\ \text{error} \end{matrix} \quad (4.9)$$

$$C_{end} = 2ns\left(2 + \frac{\pi}{2}\right)\epsilon_{end}\epsilon_0 \frac{K(\kappa_{0end})}{K(\kappa'_{0end})} \quad \begin{matrix} 6\% \\ \text{error} \end{matrix} \quad (4.10)$$

Number of Fingers	Measured Effective Capacitance at 0 volts	Measured Effective Capacitance at 90 volts	Permittivity extracted at 0V and 90 V (HFSS)	Permittivity extracted at 0V and 90 (Eq. 4.09)	Permittivity extracted at 0V and 90V (Eq. 4.10)
3	1.17 pF	0.88 pF	800-500	400-250	750-510
5	2.1 pF	1.5 pF	750-500	450-270	770-500
7	3.2 pF	2.2 pF	750-500	470-270	800-520

Number of Fingers	Measured Effective Capacitance at 0 volts	Measured Effective Capacitance at 90 volts	Permittivity extracted at 0V and 90 V (HFSS)	Permittivity extracted at 0V and 90 (Eq.4.09)	Permittivity extracted at 0V and 90V (Eq.410)
3	0.75 pF	.5 pF	350-230	160-70	350-200
5	1.4 pF	0.98 pF	350-230	180-90	360-210
7	2.1 pF	1.45 pF	350-230	200-100	370-220